

**Table 1** Axisymmetric stagnation point shear stress,  $\tau_w$ , for  $Pr = 0.27$ 

$g_o$	1.0	0.5	0.1	0.05	0.01	0.001
(a) $C = 1$	0.928	0.835	0.754	0.740	0.740	0.740
(b) $C = g_o^{-1/2}$	0.928	0.749	0.596	0.576	0.559	0.556
(a)/(b)	1.0	0.898	0.790	0.772	0.756	0.751

stress,  $\tau_w$ , for  $C = 1.0$  with that for  $C$  varying inversely as the square root of the local temperature. Calculations were performed using the method of Ref. 2.

The results of Nath ( $C = 1$ ) are related to more realistic variable  $C$  data through some function of  $g_o$  which is not known until the full problem is solved. It is thus seen that Ref. 1 is an exercise in applying a poorly chosen method to unrealistic problems. The present Comment attempts to obviate possible misinterpretations which could tempt fluid dynamicists to follow the course chosen by Nath.<sup>1</sup>

#### References

- <sup>1</sup> Nath, G., "Solution of Nonlinear Problems in Magnetofluid-dynamics and Non-Newtonian Fluid Mechanics through Parametric Differentiation," *AIAA Journal*, Vol. 11, No. 10, Oct. 1973, pp. 1429-1432.
- <sup>2</sup> Wortman, A. and Mills, A. F., "Recovery Factors in Highly Accelerated Laminar Boundary Layer Flows," *AIAA Journal*, Vol. 9, No. 7, July 1971, pp. 1415-1417.
- <sup>3</sup> Wortman, A., Ziegler, H., and Soo-Hoo, G., "Convective Heat Transfer at General Three-Dimensional Stagnation Points," *International Journal of Heat and Mass Transfer*, Vol. 14, Jan. 1971, pp. 149-152.
- <sup>4</sup> Wortman, A., "Mass Transfer in Self-Similar Boundary-Layer Flows," Rept. Aug. 1969, Northrop Corp., Hawthorne, Calif.; also Ph.D. thesis, Aug. 1969, Dept. of Engineering and Applied Science, Univ. of California, Los Angeles, Calif.

In fact, for  $c = g^{-1/2}$ , Nath<sup>3,4</sup> has obtained the solution of the above problem using a shoot and hunt scheme and the method of parametric differentiation. Further, the solution of general three-dimensional stagnation point has been obtained by Vimala<sup>5</sup> using the method of parametric differentiation for  $c = g^{-1/2}$  in contrast to  $c = 1$  as considered by Libby.<sup>6</sup> The inadequacy of solutions obtained under simplifying assumption of  $c = 1$  is well known. However, it is a common practice to use such an assumption.<sup>2,6</sup>

In view of the abovementioned results, the comment of Franks that the method is ill suited for the solutions of the boundary-layer equations is not justified. On the other hand, it can be concluded that the method of parametric differentiation is another powerful technique for solving boundary-layer equations with realistic property variations.

#### References

- <sup>1</sup> Nath, G., "Solution of Nonlinear Problems in Magnetofluid-dynamics and Non-Newtonian Fluid Mechanics through Parametric Differentiation," *AIAA Journal*, Vol. 11, No. 10, Oct. 1973, pp. 1429-1432.
- <sup>2</sup> Bush, W. B., "The Stagnation Point Boundary Layer in the Presence of an Applied Magnetic Field," *Journal of the Aerospace Sciences*, Vol. 28, No. 10, Oct. 1961, pp. 610-611.
- <sup>3</sup> Nath, G., "Compressible Axially Symmetric Laminar Boundary Layer Flow in the Stagnation Region of a Blunt Body in the Presence of Magnetic Field," *Acta Mechanica*, Vol. 12, Oct. 1971, pp. 267-273.
- <sup>4</sup> Nath, G., "Solutions of a Class of Nonlinear Two-point Boundary Value Problems in Fluid Mechanics and Magnetogasdynamics through Parametric Differentiation," *Transactions of the ASME: Journal of Fluids Engineering*, to be published.
- <sup>5</sup> Vimala, C. S., "Flow Problems in Laminar Compressible Boundary Layers," Ph.D. thesis, 1974, Dept. of Applied Mathematics, Indian Institute of Science, Bangalore, India.
- <sup>6</sup> Libby, P. A., "Heat and Mass Transfer at a General Three-Dimensional Stagnation Point," *AIAA Journal*, Vol. 5, No. 3, March 1967, pp. 507-517.

## Reply by Author to W. J. Franks

G. NATH\*

Indian Institute of Science, Bangalore, India

IN Ref. 1, an application of the method of parametric differentiation to the solutions of boundary-layer equations in magnetofluid-dynamics and in non-Newtonian fluid mechanics was presented. The aim of the analysis was to show that the method can be applied successfully to complex flowfields containing a number of parameters. For the first problem, it has been pointed out by Bush<sup>2</sup> and also verified by the present author that the usual method of solving two-point boundary-value problems, i.e., the method of shoot and hunt fails for large value of the magnetic parameter  $M$  ( $M > 10$ ) even under the simplifying assumptions of  $Pr = 1$  and constant density-viscosity product, i.e.,  $c = \rho\mu/\rho_e\mu_e = 1$ . In our analysis, we assumed  $c = 1$  because we wanted to compare our results with the corresponding results obtained by a shoot and hunt scheme which were available to the author for the case  $c = 1$ . It may be remarked that the present method of solution is valid even for  $M = 100$ , but the results for  $M > 10$  were not tabulated in Ref. 1 because no comparison could be made.

Received March 7, 1974.

Index category: Boundary Layers and Convective Heat Transfer—Laminar.

\* Assistant Professor, Department of Applied Mathematics.

## Errata

### A Study of Compressible Potential and Asymptotic Viscous Flows for Corner Region

K. N. GHIA AND R. T. DAVIS

University of Cincinnati, Cincinnati, Ohio

[AIAA J 12, 355-359 (1974)]

EQUATION (13) should read:

$$U_{1,c} = -\frac{\beta}{2m} \left[ \frac{[(x^2 + m^2 y^2)^{1/2} - x]^{1/2}}{(x^2 + m^2 y^2)^{1/2}} + \frac{[(x^2 + m^2 z^2)^{1/2} - x]^{1/2}}{(x^2 + m^2 z^2)^{1/2}} \right] \quad (13)$$

The last paragraph in the subsection "Subsonic Flow" should read:

For the compressible flow velocities given by Eqs. (13-15), the quantity  $\beta$  has the same significance as expressed in Eq. (5), although its numerical value will be, in general, different from that for incompressible flow.

Received April 15, 1974.

Index categories: Supersonic and Hypersonic Flow; Jets, Wakes, and Viscid-Inviscid Flow Interactions.